

APPENDIX I—PERFORMANCE DATA

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part 1—INTRODUCTION

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SCOPE.

The purpose of this appendix is two-fold: it provides EC-121D, H, Q and C-121G aircraft performance information needed for flight planning under standard and non-standard conditions, and it also provides information needed to check aircraft and engine performance in flight. The purpose is accomplished by an eight-part arrangement of data, and except as noted below, covers both aircraft in each part. Each part relates either to a particular phase of flight or summarizes a particular type of information. For example, Part 2 presents engine operating data which applies to all phases of operation. Detailed engine limits, power available, and fuel flow characteristics are given there. Part 3 contains data needed for takeoff planning, such as maximum power prediction, critical field lengths, speed schedules, and check data so that aircraft speed can be compared with predicted performance during the take-off run. Parts 5 and 6 deviate from the dual coverage concept in that Part 5 is applicable only to cruising operation of the EC-121 and Part 6 applies only to the C-121G. Silhouettes in the upper corners of the charts are used to indicate the model or models to which charts are applicable. The procedures to be followed in using the charts are given with discussions of the data. Numerical examples and solutions are also provided.

CARBURETOR AIR SCOOPS.

All performance data shown in this appendix reflects operation with the overcowl (Mark V-A) ram air scoops installed with the ram air doors open. Operation with the ram doors closed can result in a cruise speed loss of up to 2 knots IAS under part-throttle conditions.

DATA BASIS.

EC-121R performance data is based on flight tests and performance reports for C-121C and G aircraft and commercial models 1049C, G, and H. Receipt of this material has extended over a period of several years. The release date on the performance charts represents the approximate time of its reevaluation for applicability to this flight manual.

FUEL AND FUEL DENSITY.

Aircraft and engine performance shown is representative of normal operation with 115/145 grade fuel in all cases except where specifically noted. This fuel has a nominal density of 6 pounds per gallon (US).

AIRSPEED AND ALTIMETER CORRECTION CHARTS.

Airspeed and altitude readings obtained directly from flight instruments should be corrected prior to use to account for the mechanical errors in individual instruments and the position errors due to locations selected for the static holes. An additional correction to airspeed readings should be made to account for compressibility effects due to altitude. Position and compressibility error correction charts are provided for this purpose in this part of the Appendix. Note that they give the correction to be applied, not the error. Individual instrument corrections cannot be supplied here, but should be made available by periodic bench calibrations and supplied on calibration cards for your instruments in use. Particular attention should be given to the altitude correction as it may mean the difference between clearing an obstacle or not. See the altitude relationship sample problem.

Note

The physical condition of the flush-static and pitot-head pressure sources is quite important as it affects the accuracy of the position error corrections. These sources should be inspected frequently, heads kept in alignment, and be free of water, dirt, leaks, metal burrs, etc., which might result in serious malfunction of the airspeed system.

SYMBOLS AND DEFINITIONS.

| | | | |
|-------------------|---|-----------|--|
| IAS | Indicated airspeed—The speed value read from an airspeed indicator. Where this symbol (IAS) is used on performance charts, mechanical error is assumed zero or applied. | σ | Sigma—Ratio of ambient air density to standard day sea level air density. |
| BAS | Basic airspeed—The indicated airspeed reading corrected for instrument mechanical error. | OATI | Indicated outside air temperature—Value read from air temperature gage. |
| CAS | Calibrated airspeed—The airspeed obtained by applying the position error correction to basic airspeed. | BAT | Basic air temperature—Indicated outside air temperature corrected for instrument mechanical error. |
| EAS | Equivalent airspeed—The airspeed obtained by applying the altitude compressibility correction to calibrated airspeed. Also obtained by dividing true airspeed by $1/\sqrt{\sigma}$. | OATC | Corrected outside air temperature—Air temperature obtained by correcting BAT for the temperature rise which accompanies adiabatic compression. |
| TAS | True airspeed—Speed of aircraft relative to the air through which it is flying ($EAS \times 1/\sqrt{\sigma}$). | CAT | Carburetor air temperature. |
| V_p | Airspeed position correction. | CHT | Cylinder head temperature. |
| V_c | Airspeed compressibility correction. | RPM | Revolutions Per Minute—Engine rotational speed. |
| V_s | Stall speed at zero thrust. | BMEP | Brake Mean Effective Pressure—BMEP gage reading corrected for instrument error. |
| V_G | Groundspeed—Speed of the aircraft relative to the ground over which it flies. | BHP | Brake Horsepower—Engine power delivered for propulsion. $BHP = RPM \times BMEP/236$ for 3350-cubic-inch-displacement engines. |
| V_{MCG} | Minimum control speed (ground) with a failed engine and maximum power on the operative engines. | MAP | Manifold absolute pressure. |
| V_{MCA} | Minimum control speed (air) with a failed engine, maximum power on operative engines, constant heading, and a bank angle equal or less than 5°. | in. Hg | Inches of mercury. |
| ICAO | International Civil Aviation Organization. | R.T. | Reverse thrust. |
| H_p | Pressure altitude—That value obtained after correcting an altimeter reading for instrument and position errors. | F.T. | Full-throttle engine performance. |
| H_d | Density altitude—That value obtained from the Density Altitude Chart at which air density at the existing pressure altitude and temperature equals air density as defined by the ICAO for standard atmospheric condition. | METO | Maximum except takeoff power. |
| SL | Sea level. | lb/hr/eng | Pound per hour per engine (fuel flow). |
| $1/\sqrt{\sigma}$ | Smoe factor. | R/C | Rate of climb. |
| | | Ft/Min | Feet per minute (fpm). |
| | | RCR | Runway condition reading. |
| | | RSC | Runway surface condition. |

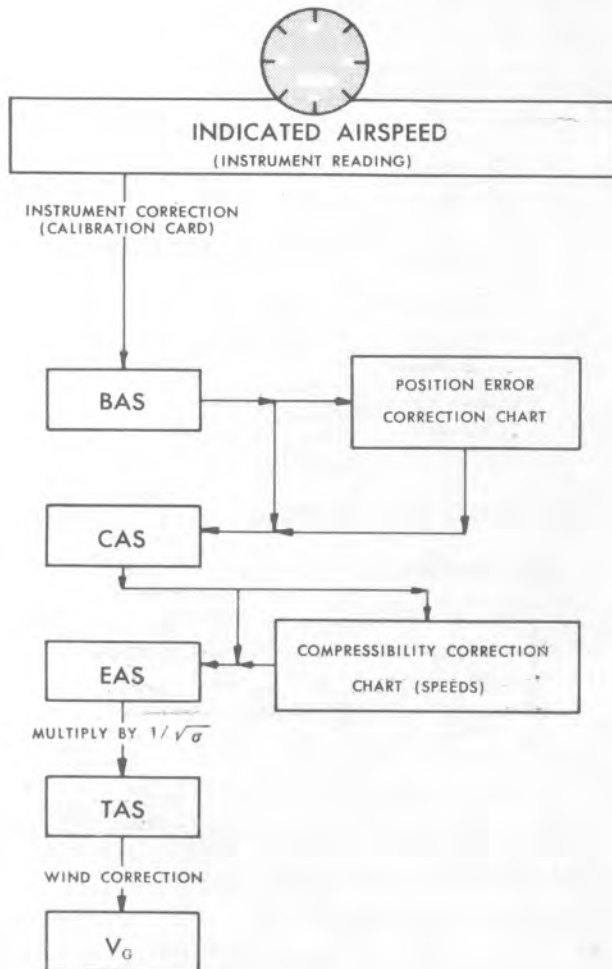
SAMPLE PROBLEMS—USE OF STANDARD CHARTS.

The examples illustrate the use of the standard correction charts and the sequence to be followed. The cases are for level flight conditions that provide the stabilized instrument readings shown. Instrument calibrations used are assumed values. The instrument calibration cards should be employed when available; otherwise, assume zero error.

TEMPERATURE CORRECTION AND CONVERSION CHARTS.

At normal flight speeds, outside air temperature is less than the value indicated by the flight instruments. This is due to the temperature rise which occurs when ram air surrounds the sensing element. The air is heated by compression to nearly 100 percent of the possible adiabatic rise. Figures A1-7 and A1-8 provide corrections which must be made to the indicated value to obtain correct true ambient air temperature. Corrections for individual instruments errors should be applied first, of course. Figure A1-9 is provided as a convenience for converting from Centigrade to Fahrenheit temperature.

SPEED RELATIONSHIP



SAMPLE PROBLEMS.

Static System Used No. 2
 Instrument Panel Pilot
 Wing Flaps and Gear Up

Problem 1: To find calibrated airspeed (CAS).

Indicated Airspeed (IAS) 184 Knots
 (Instrument reading)
 Instrument Correction (assumed) -2
 (Obtain from calibration card)
 Basic Airspeed (BAS) 182 Knots
 (IAS + calibration card correction)
 Position Error Correction +3.0
 (Use figure A1-2, V_p)
 Calibrated Airspeed (CAS) 185 Knots
 (BAS + ΔV_p)

Problem 2: To find equivalent airspeed (EAS).

Altimeter Reading 20,250 ft
 (From instrument set at 29.92 in. Hg)
 Instrument Correction -340 ft
 (Obtain from calibration card)
 Indicated Pressure Altitude 19,910 ft
 (Instrument reading + correction)
 Position Error Correction +90
 (From figure A1-4, ΔH_p)
 Pressure Altitude (H_p) 20,000 ft
 (Indicated pressure altitude + ΔH_p)
 Airspeed Compressibility Correction -2.0
 (Use figure A1-5 or A1-6, find ΔV_c)
 Equivalent Airspeed (EAS) 183 Knots
 (CAS + ΔV_c)

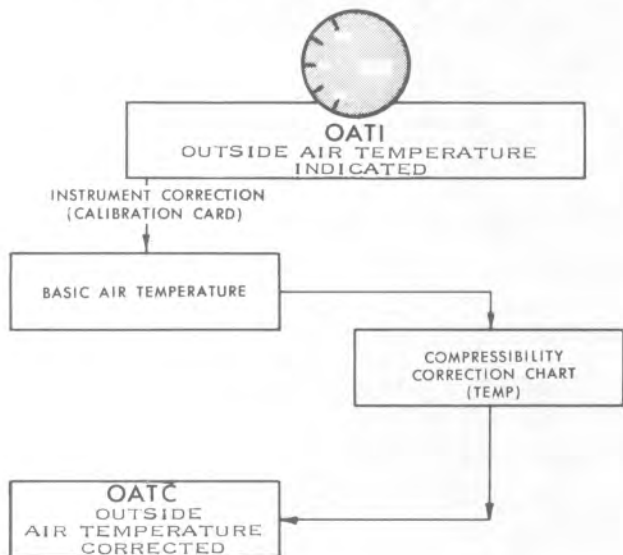
Problem 3: To find true airspeed (TAS).

Equivalent Airspeed 183 Knots
 (From problem above)
 $1/\sqrt{\sigma}$ (H_i at 21,050 ft) 1.395
 (Use figure A1-11 or A1-12)
 True Airspeed (TAS) 255 Knots
 (EAS $\times 1/\sqrt{\sigma}$)

STANDARD ATMOSPHERE TABLE.

The Standard Atmosphere Table (figure A1-10), presented for reference purposes, shows the standard variation of temperature, pressure, and density with altitude. It is based on definitions adopted by the ICAO, and supersedes data previously issued by the NACA.

TEMPERATURE RELATIONSHIP



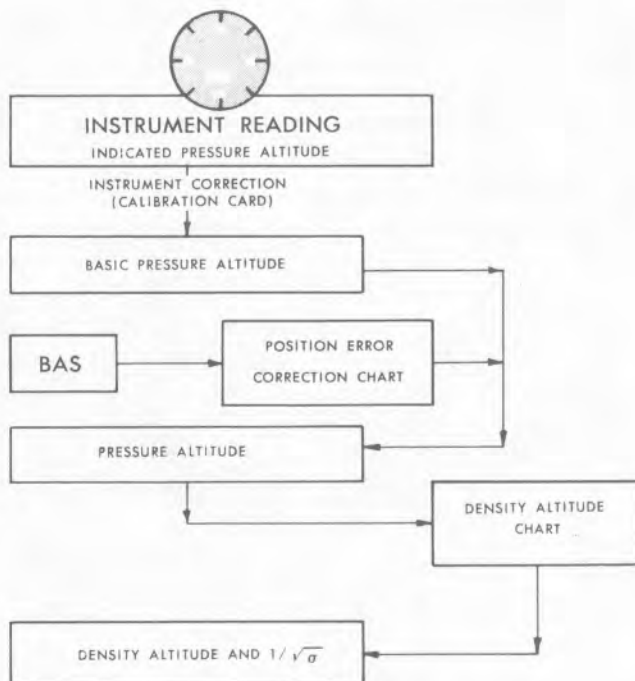
SAMPLE PROBLEM.

- Indicated Outside Air Temperature -4°C
(From OATI instrument)
- Instrument Correction (assumed) -3°C
(Obtained from calibration card)
- Basic Air Temperature -7°C
(Instrument reading + correction)
- Compressibility Correction -8.5°C
(Use figure A1-7 or A1-7, read ΔT)
- Corrected Outside Air Temperature
(OATC) -15.5°C
(Basic air temperature + ΔT)
- Temperature Conversion +4°F
(Use figure A1-9, read OATC in °F)

DENSITY ALTITUDE CHART.

The Density Altitude Chart, figure A1-12, is based on the ICAO definition of standard atmosphere. It can be used directly to find density altitude (H_d) and density ratio when pressure altitude (H_p) and ambient air temperature (OATC) are given. Note the accuracy with which air temperature should be known. An error of 5°C will give an error in H_d of about 550 feet. The resultant error in $1/\sqrt{\sigma}$ will be about 1%, an error which would be reflected in computing true airspeed. Pressure altitude should be read from an instrument set at 29.92 in. Hg, the standard pressure at sea level.

ALTITUDE RELATIONSHIP



To fly at assigned flight level of 20,000 ft pressure altitude, 184 knots IAS, indicate 20,250 ft on altimeter to account for instrument and position error.

20,000 ft level flight pressure altitude
(aircraft indicating 20,250 ft)



Aircraft indicating 20,000 ft
(250 ft error in altitude)



SAMPLE PROBLEMS.

- Static System Used No. 2
- Instrument Panel Pilot
- Wing Flaps and Gear Up

Problem 1: To find pressure altitude (H_p).

- Altimeter Reading 20,250 ft
(From instrument set at 29.92 in. Hg)
- Instrument Correction (assumed) -340 ft
(Obtain from calibration card)
- Indicated Pressure Altitude 19,910 ft
(Instrument reading + correction)
- Position Error Correction +90
(From figure A1-4, Δ H_p)
- Pressure Altitude (H_p) 20,000 ft
(Indicated pressure altitude + position error correction)

Problem 2: To find density altitude (H_d) and $1/\sqrt{\sigma}$.

Density Altitude (H_d)21,050 ft
 (From figure A1-12, read H_d at the intersection of pressure altitude, 20,000, and OATC, -15.5°C)

$1/\sqrt{\sigma}$ 1.395
 (From figure A1-11 or A1-12, read $1/\sqrt{\sigma}$ opposite density altitude 21,050)

PSYCHROMETRIC CHART.

A Psychrometric Chart (figure A1-13) is included. This chart may be used to determine the dewpoint temperature value which is used in predicting maximum power available. The dewpoint may be determined with wet- and dry-bulb temperatures, vapor pressure, or specific humidity combined with the pressure altitude.

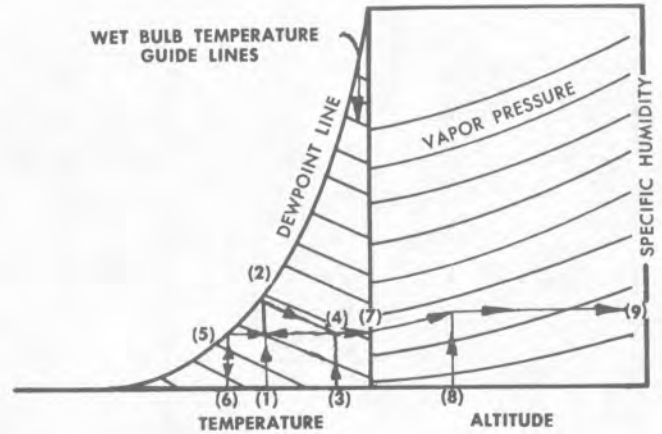
SAMPLE PROBLEM.

Use of the Psychrometric Chart (figure A1-13) provides dewpoint temperatures for prediction of maximum power for takeoff. The chart can also be used to find vapor pressure, specific humidity, and relative humidity.

If wet- and dry-bulb temperatures are given, find dewpoint by steps 1-6 in the following sequence. Enter the chart with wet-bulb temperature (1) and move to the dewpoint base line (2). Proceed diagonally parallel to a wet-bulb guide line nearest the pressure altitude to point (4) located above the dry-bulb temperature (3). Move left horizontally to the dewpoint line (5) and read dewpoint below at position (6). If wet-bulb temperature is 70°F and dry-bulb temperature is 95°F , the dewpoint is 57.7°F .

If vapor pressure only is given, enter the chart with vapor pressure at (7) and follow the step sequence 7, 5, 6. Dewpoint is 57.7°F when vapor pressure is 0.495.

USE OF THE PSYCHROMETRIC CHART



Follow step sequence 9, 8, 7, 5, 6 when specific humidity and pressure altitude are given. Proceed horizontally from specific humidity (9) to pressure altitude (8), then parallel to a vapor pressure guide line to the vapor pressure base line (7). Continue horizontally to the dewpoint line (5) and vertically to dewpoint at (6). Dewpoint is 57.7°F for a specific humidity of 0.012 and 3000-foot pressure altitude.

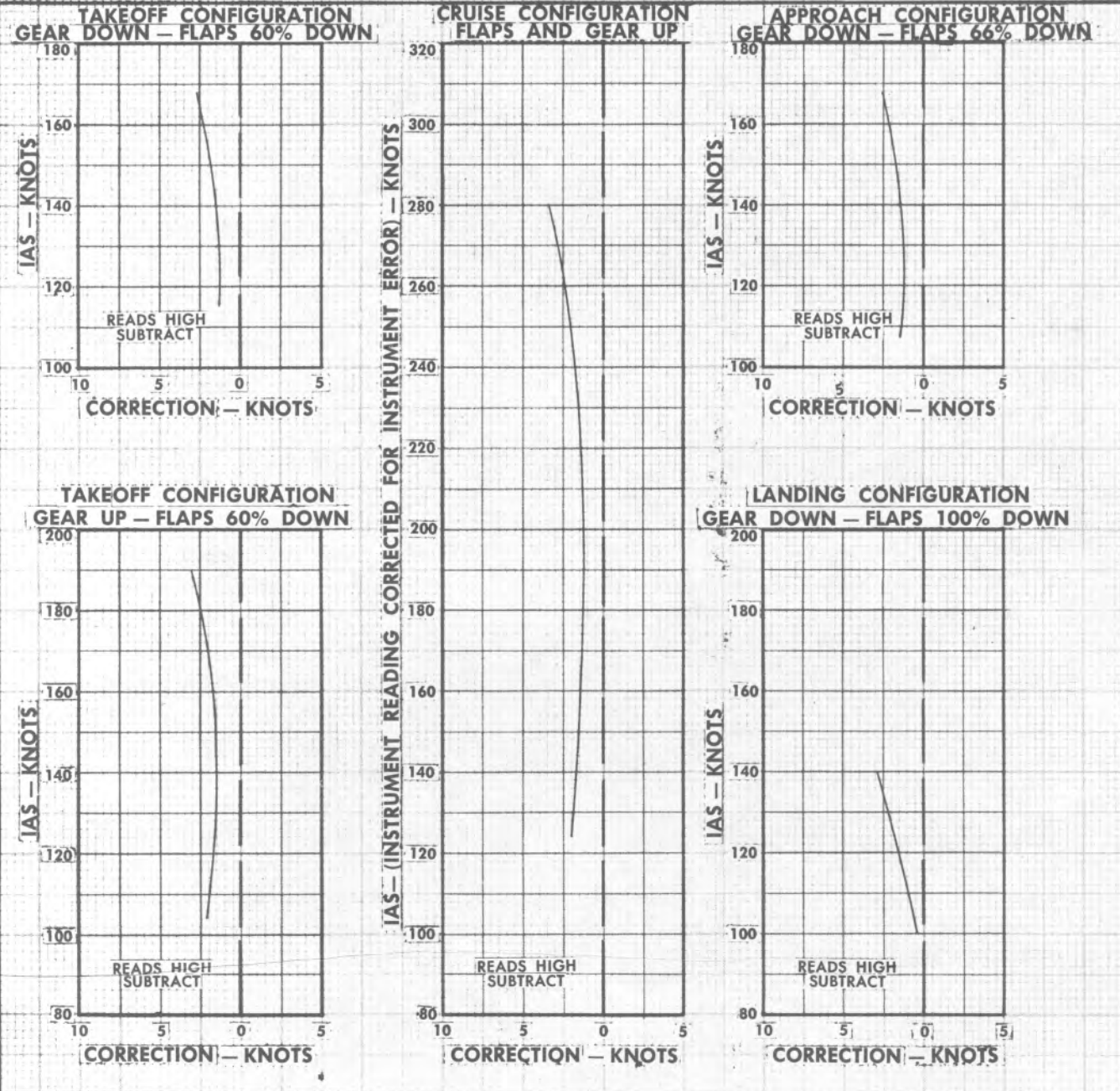
Relative humidity can be used with dry-bulb temperature to find the dewpoint. For 80% rh and 64°F dry-bulb temperature, locate a position 80% of the vertical distance from the temperature line to the dewpoint line. Proceed horizontally to the dewpoint line (5) and read dewpoint below at (6) of 57.7°F , or 14°C . Wet-bulb temperature would be 60°F for these conditions, since this is the intersection of a wet-bulb guide line drawn from (5) to the 80% relative humidity line.

AIRSPEED POSITION ERROR CORRECTION

**NO. 1 STATIC SYSTEM
POWER FOR LEVEL FLIGHT**

MODEL: EC-121R/C-121G
DATA AS OF: 31 MARCH 1967
DATA BASIS: FLIGHT TEST

ENGINE: (4) R3350-93A
PROPS: HAM. STD. 43H60/6959B-O



Total Head Location: 4 inches below fuselage skin, to the left of bottom centerline, at fuselage station 155.70
Flush Static Location: fuselage station 335.70, water line 194.19 (right and left teed together)

Figure A1-1

AIRSPEED POSITION ERROR CORRECTION

NO. 2 STATIC SYSTEM
POWER FOR LEVEL FLIGHT

MODEL: EC-121R/C-121G

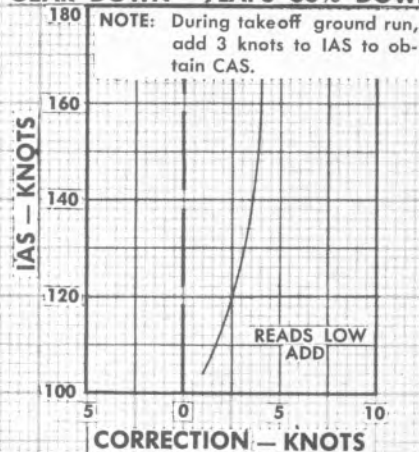
DATA AS OF: 31 MARCH 1967

DATA BASIS: FLIGHT TEST

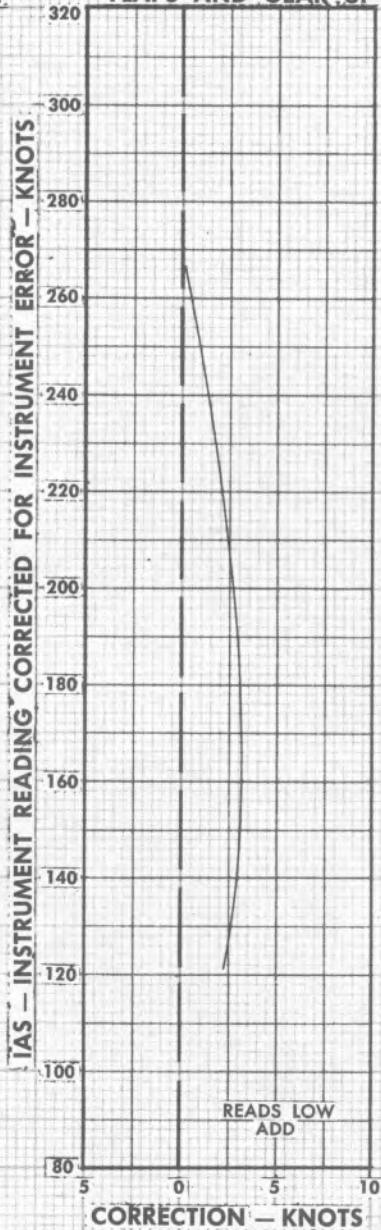
ENGINE: (4) R3350-93A

PROPS: HAM. STD. 43H60/6959B-O

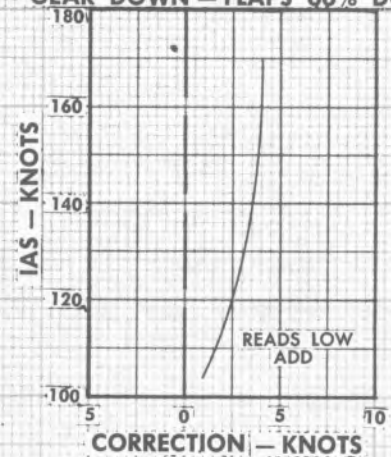
TAKEOFF CONFIGURATION
GEAR DOWN - FLAPS 60% DOWN



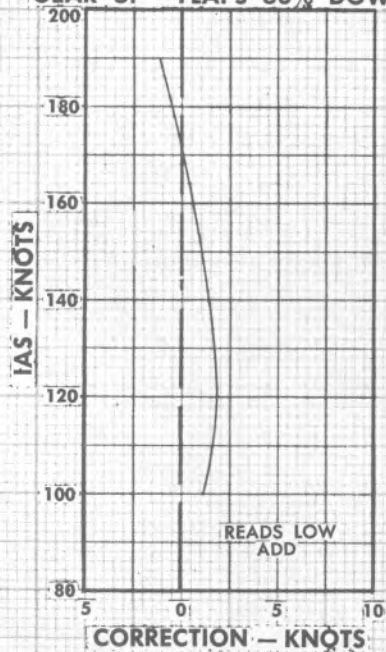
CRUISE CONFIGURATION
FLAPS AND GEAR UP



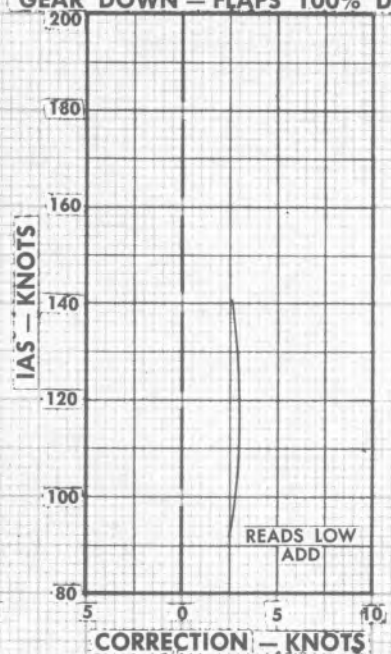
APPROACH CONFIGURATION
GEAR DOWN - FLAPS 66% DOWN



TAKEOFF CONFIGURATION
GEAR UP - FLAPS 60% DOWN



LANDING CONFIGURATION
GEAR DOWN - FLAPS 100% DOWN



Total Head Location: 4 inches below fuselage skin, to the left of bottom centerline, at fuselage station 155.70
Flush Static Location: fuselage station 155.00, water line 214.08 (right and left tied together)

Figure A1-2

ALTIMETER POSITION ERROR CORRECTION

NO. 1 FLUSH STATIC SYSTEM
POWER FOR LEVEL FLIGHT

MODEL: EC-121R/C-121G

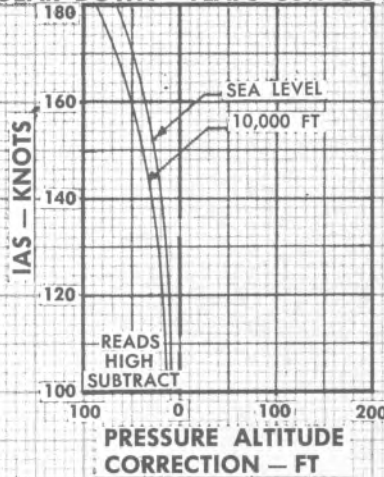
DATA AS OF: 31 MARCH 1967

DATA BASIS: FLIGHT TEST

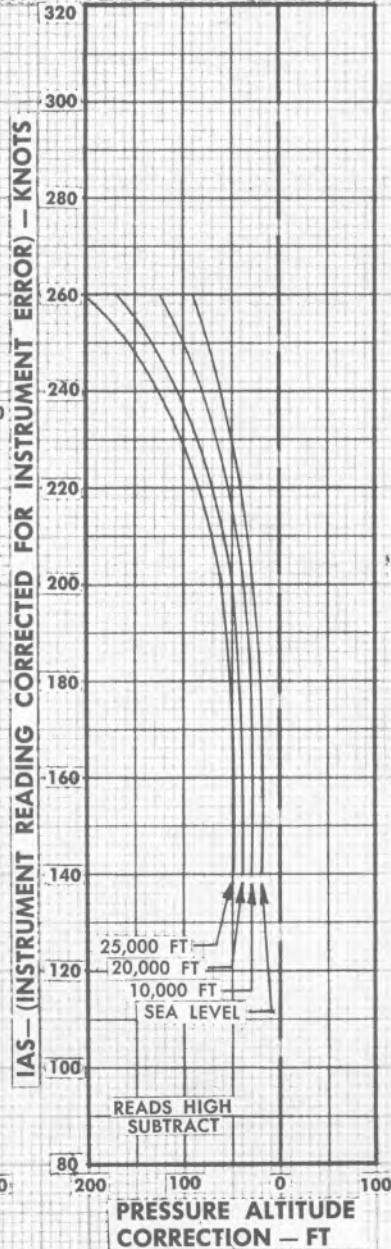
ENGINE: (4) R3350-93A

PROPS: HAM. STD. 43H60/6959B-O

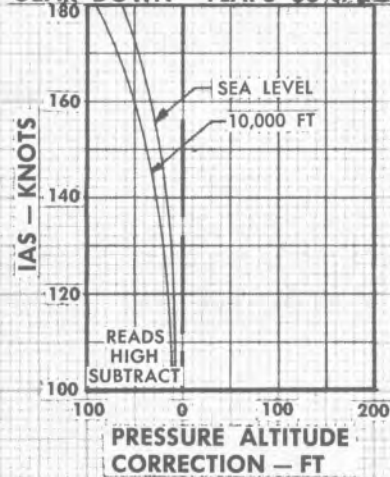
TAKEOFF CONFIGURATION
GEAR DOWN - FLAPS 60% DOWN



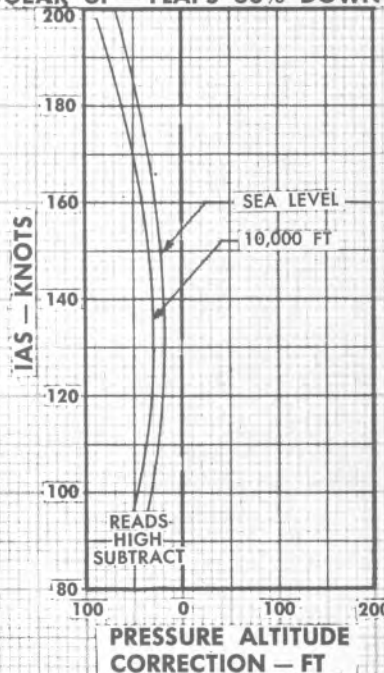
CRUISE CONFIGURATION
FLAPS AND GEAR UP



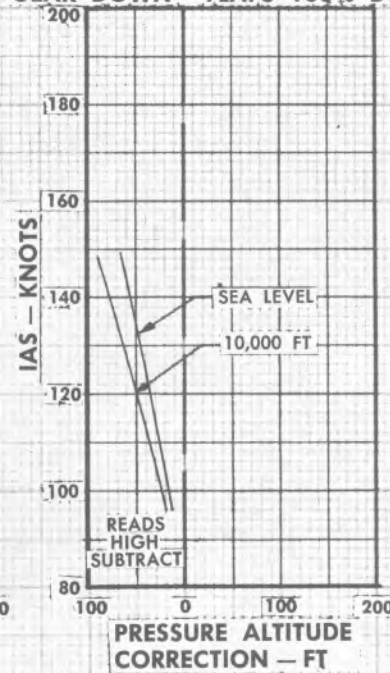
APPROACH CONFIGURATION
GEAR DOWN - FLAPS 66% DOWN



TAKEOFF CONFIGURATION
GEAR UP - FLAPS 60% DOWN



LANDING CONFIGURATION
GEAR DOWN - FLAPS 100% DOWN



Flush Static Location: fuselage station 335.70, water line 194.19
(right and left teed together)

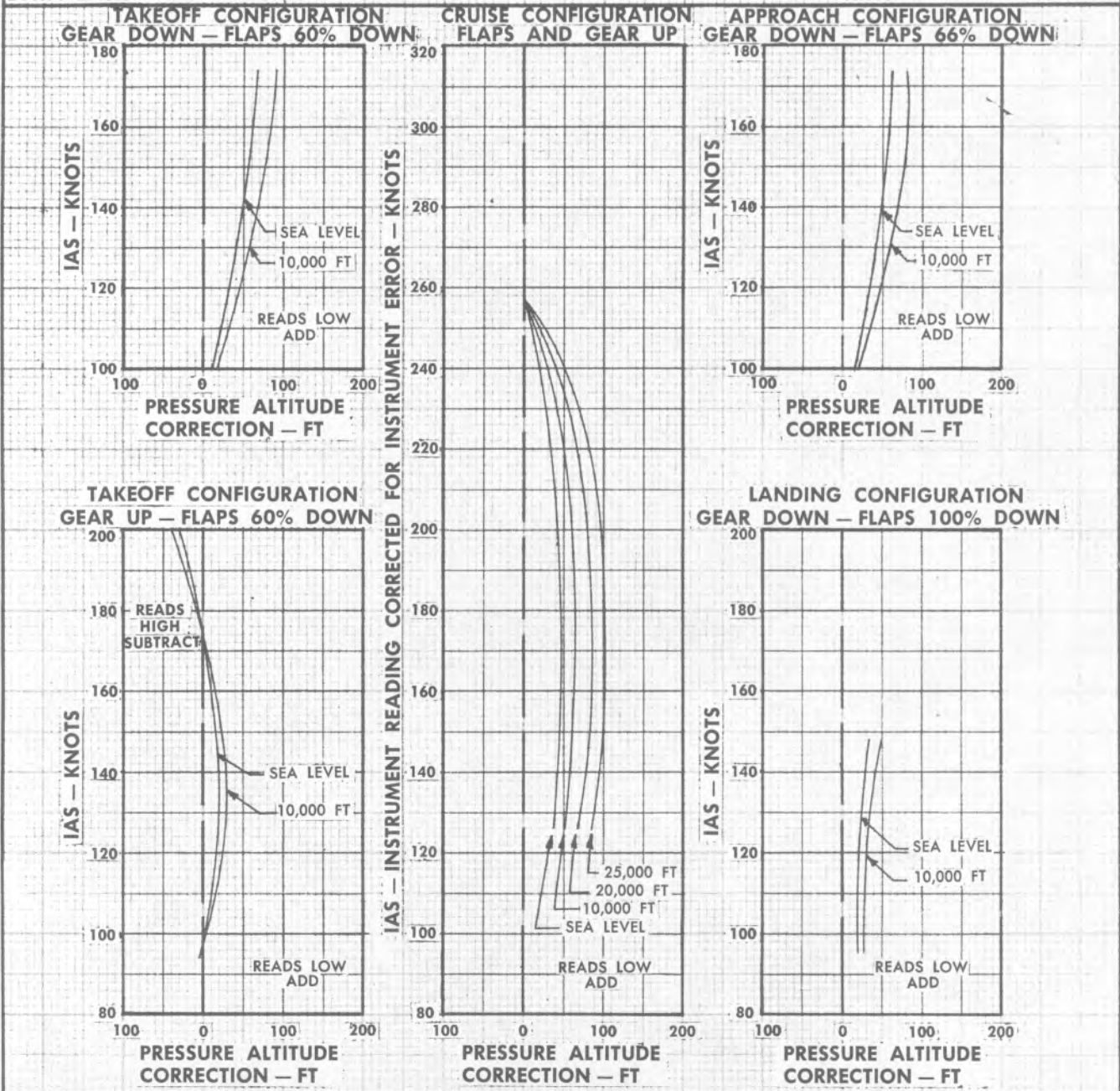
Figure A1-3

ALTIMETER POSITION ERROR CORRECTION

NO. 2 FLUSH STATIC SYSTEM
POWER FOR LEVEL FLIGHT

MODEL: C-121C/G
DATA AS OF: 15 SEPTEMBER 1962
DATA BASIS: FLIGHT TEST

ENGINE: (4) R3350-93
PROPS: HAM. STD. 43H60/6959B-O



REMARKS: Flush Static (L. and R. tied together) location: Fus. sta. 155.0
W.L. 214.08.

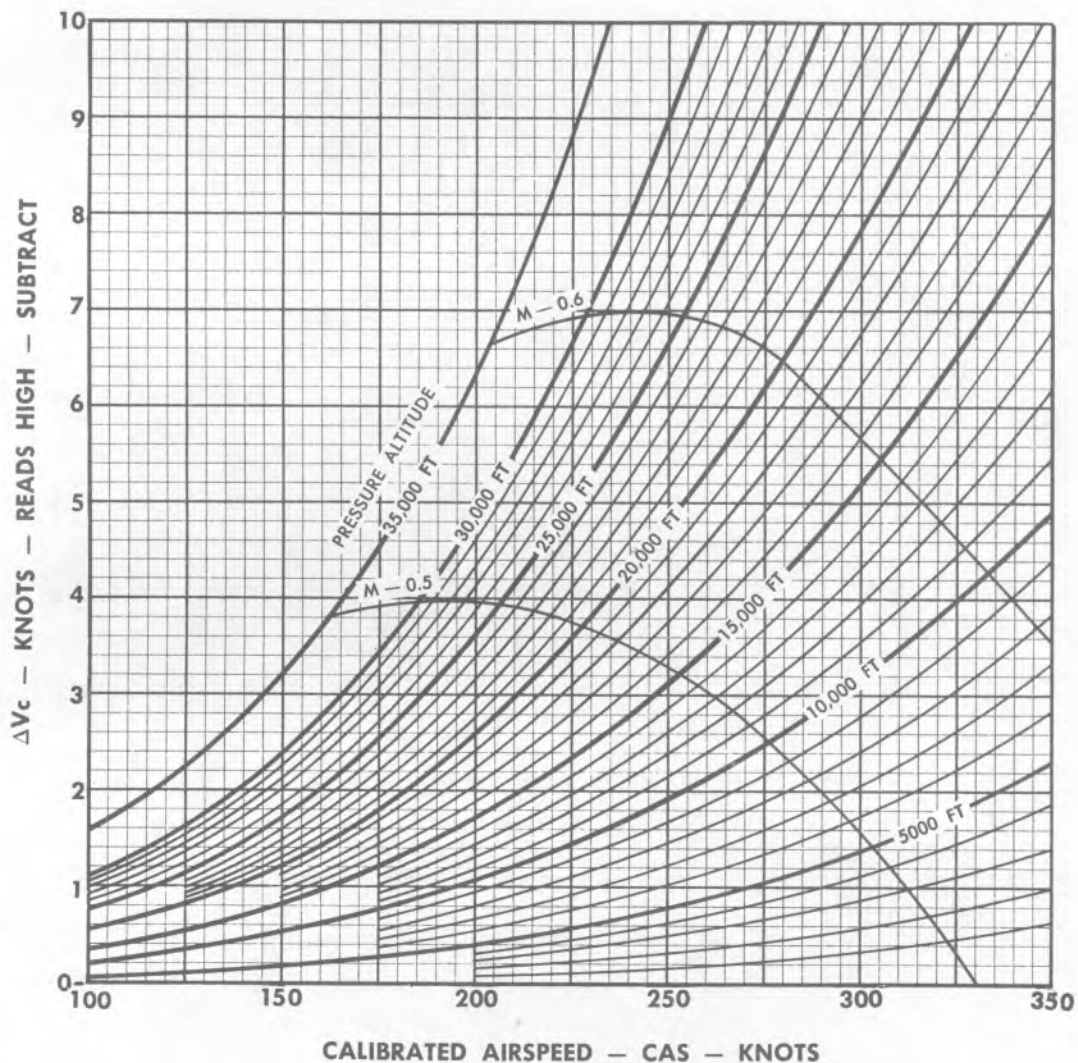
Figure A1-4

AIRSPEED COMPRESSIBILITY CORRECTION CHART

CORRECTION TO CALIBRATED AIRSPEED TO OBTAIN EQUIVALENT AIRSPEED

REMARKS:

1. Equivalent airspeed (EAS) equals IAS corrected for instrument error, installation error, and the altitude compressibility correction shown above.
2. True speed through the air (TAS) equals $(EAS) \times 1/\sqrt{\sigma}$



EAS = CAS - ΔV_c
 TAS = $EAS \times 1/\sqrt{\sigma}$
 M = MACH NUMBER
 $\sigma = \rho/\rho_0$

Figure A1-5

AIRSPEED COMPRESSIBILITY CORRECTION TABLE

Add correction to calibrated airspeed to obtain equivalent airspeed

| | CALIBRATED AIRSPEED — KNOTS | | | | | | | | | | | | |
|-----------|-----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 150 | 160 | 170 | 180 | 190 | 200 | 210 | 220 | 230 | 240 | 250 | 260 | |
| Sea Level | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -0.5 |
| 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -0.5 | -0.5 | -0.5 | -0.5 |
| 3 | 0 | 0 | 0 | 0 | 0 | 0 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 |
| 4 | 0 | 0 | 0 | 0 | 0 | 0 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -1.0 |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 |
| 6 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 |
| 7 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 |
| 8 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -1.5 |
| 9 | -0.5 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -2.0 | -2.0 |
| 10 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -2.0 | -2.0 |
| 11 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.0 | -2.0 | -2.0 | -2.5 |
| 12 | -0.5 | -0.5 | -0.5 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -2.0 | -2.0 | -2.0 | -2.5 | -2.5 |
| 13 | -0.5 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -1.5 | -1.5 | -2.0 | -2.0 | -2.0 | -2.5 | -3.0 |
| 14 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -2.0 | -2.0 | -2.0 | -2.5 | -2.5 | -3.0 | -3.0 |
| 15 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.0 | -2.0 | -2.0 | -2.5 | -2.5 | -3.0 | -3.5 |
| 16 | -1.0 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.0 | -2.5 | -3.0 | -3.0 | -3.0 | -3.5 | -4.0 |
| 17 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.0 | -2.0 | -2.5 | -3.0 | -3.0 | -3.0 | -4.0 | -4.0 |
| 18 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.5 | -2.5 | -2.5 | -3.0 | -3.5 | -3.5 | -4.0 | -4.5 |
| 19 | -1.0 | -1.0 | -1.0 | -1.5 | -2.0 | -2.5 | -2.5 | -3.0 | -3.5 | -3.5 | -3.5 | -4.5 | -5.0 |
| 20 | -1.5 | -1.5 | -1.5 | -1.5 | -2.0 | -2.5 | -3.0 | -3.0 | -3.0 | -4.0 | -4.0 | -5.0 | -5.5 |
| 21 | -1.5 | -1.5 | -1.5 | -2.0 | -2.5 | -3.0 | -3.0 | -3.5 | -4.0 | -4.5 | -4.5 | -5.0 | -6.0 |
| 22 | -1.5 | -1.5 | -2.0 | -2.0 | -2.5 | -3.0 | -3.5 | -4.0 | -4.5 | -5.0 | -5.0 | -5.5 | -6.0 |
| 23 | -1.5 | -2.0 | -2.0 | -2.0 | -2.5 | -3.0 | -3.5 | -4.0 | -4.5 | -5.0 | -5.0 | -6.0 | -6.5 |
| 24 | -2.0 | -2.0 | -2.0 | -2.5 | -3.0 | -3.5 | -4.0 | -4.5 | -5.0 | -5.5 | -5.5 | -6.5 | -7.0 |
| 25 | -2.0 | -2.0 | -2.0 | -2.5 | -3.0 | -3.5 | -4.0 | -4.5 | -5.0 | -6.0 | -6.0 | -6.5 | -7.5 |

PRESSURE ALTITUDE — 1000 FEET

AIRSPEED POSITION ERROR CORRECTION — WING FLAPS AND GEAR UP

Add correction to indicated airspeed to obtain calibrated airspeed.

| IAS — Knots | 120 | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 | 210 | 220 | 230 |
|--------------|------|------|------|------|------|------|------|------|------|------|------|------|
| No. 1 Static | -2.0 | -1.5 | -1.5 | -1.5 | -1.5 | -1.0 | -1.0 | -1.0 | -1.5 | -1.5 | -1.5 | -2.0 |
| No. 2 Static | 2.0 | 2.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 2.5 | 2.0 | 2.0 |

Figure A1-6

TEMPERATURE COMPRESSIBILITY CORRECTION TABLE DEGREES CENTIGRADE

Add correction to indicated temperature to obtain approximate free-air temperature

| | | CALIBRATED AIRSPEED — KNOTS | | | | | | | | | | | |
|-------------------------------|-----------|-----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | | 150 | 160 | 170 | 180 | 190 | 200 | 210 | 220 | 230 | 240 | 250 | 260 |
| PRESSURE ALTITUDE — 1000 FEET | Sea Level | -3 | -3 | -4 | -4 | -5 | -5 | -6 | -6 | -7 | -8 | -8 | -9 |
| | 1 | -3 | -3 | -4 | -4 | -5 | -5 | -6 | -7 | -7 | -8 | -9 | -9 |
| | 2 | -3 | -3 | -4 | -4 | -5 | -6 | -6 | -7 | -7 | -8 | -9 | -9 |
| | 3 | -3 | -3 | -4 | -5 | -5 | -6 | -6 | -7 | -8 | -8 | -9 | -10 |
| | 4 | -3 | -3 | -4 | -5 | -5 | -6 | -6 | -7 | -8 | -9 | -9 | -10 |
| | 5 | -3 | -4 | -4 | -5 | -5 | -6 | -7 | -7 | -8 | -9 | -9 | -10 |
| | 6 | -4 | -4 | -4 | -5 | -5 | -6 | -7 | -8 | -8 | -9 | -10 | -10 |
| | 7 | -4 | -4 | -5 | -5 | -6 | -6 | -7 | -8 | -8 | -9 | -10 | -10 |
| | 8 | -4 | -4 | -5 | -6 | -6 | -7 | -7 | -8 | -9 | -10 | -10 | -11 |
| | 9 | -4 | -4 | -5 | -6 | -6 | -7 | -7 | -8 | -9 | -10 | -11 | -11 |
| | 10 | -4 | -4 | -5 | -6 | -6 | -7 | -8 | -8 | -9 | -10 | -11 | -12 |
| | 11 | -4 | -4 | -5 | -6 | -6 | -7 | -8 | -9 | -9 | -10 | -11 | -12 |
| | 12 | -4 | -4 | -5 | -6 | -7 | -7 | -8 | -9 | -10 | -11 | -12 | -13 |
| | 13 | -4 | -5 | -6 | -6 | -7 | -8 | -8 | -9 | -10 | -11 | -12 | -13 |
| | 14 | -5 | -5 | -6 | -7 | -7 | -8 | -9 | -10 | -11 | -12 | -12 | -14 |
| | 15 | -5 | -5 | -6 | -7 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 |
| | 16 | -5 | -5 | -6 | -7 | -8 | -8 | -9 | -11 | -11 | -12 | -13 | -14 |
| | 17 | -5 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 |
| | 18 | -5 | -5 | -7 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 |
| | 19 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 | -16 |
| | 20 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 | -17 |
| | 21 | -6 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -15 | -16 | -17 |
| | 22 | -6 | -7 | -8 | -8 | -10 | -10 | -12 | -13 | -14 | -15 | -16 | -18 |
| | 23 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -16 | -17 | -19 |
| | 24 | -6 | -7 | -8 | -9 | -11 | -11 | -13 | -14 | -15 | -16 | -17 | -19 |
| 25 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -16 | -17 | -18 | -20 | |

AIRSPEED POSITION ERROR CORRECTION — WING FLAPS AND GEAR UP

Add correction to indicated airspeed to obtain calibrated airspeed

| IAS — Knots | 120 | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 | 210 | 220 | 230 |
|--------------|------|------|------|------|------|------|------|------|------|------|------|------|
| No. 1 Static | -2.0 | -2.0 | -1.5 | -1.5 | -1.5 | -1.5 | -1.5 | -1.5 | -1.5 | -1.5 | -1.5 | -2.0 |
| No. 2 Static | 2.0 | 2.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 2.5 | 2.0 | 2.0 |

Figure A1-7

TEMPERATURE COMPRESSIBILITY CORRECTION CHART

CORRECTION TO INDICATED AMBIENT AIR TEMPERATURE
TO OBTAIN APPROXIMATE FREE AIR TEMPERATURE

- REMARKS: 1. 100% adiabatic temperature rise assumed.
 2. Indicated temperatures read high.
 3. Data based on NACA standard day conditions.
 4. Sensing element: resistance bulb located in externally ventilated box at fus sta 220.65 w l 179.71.

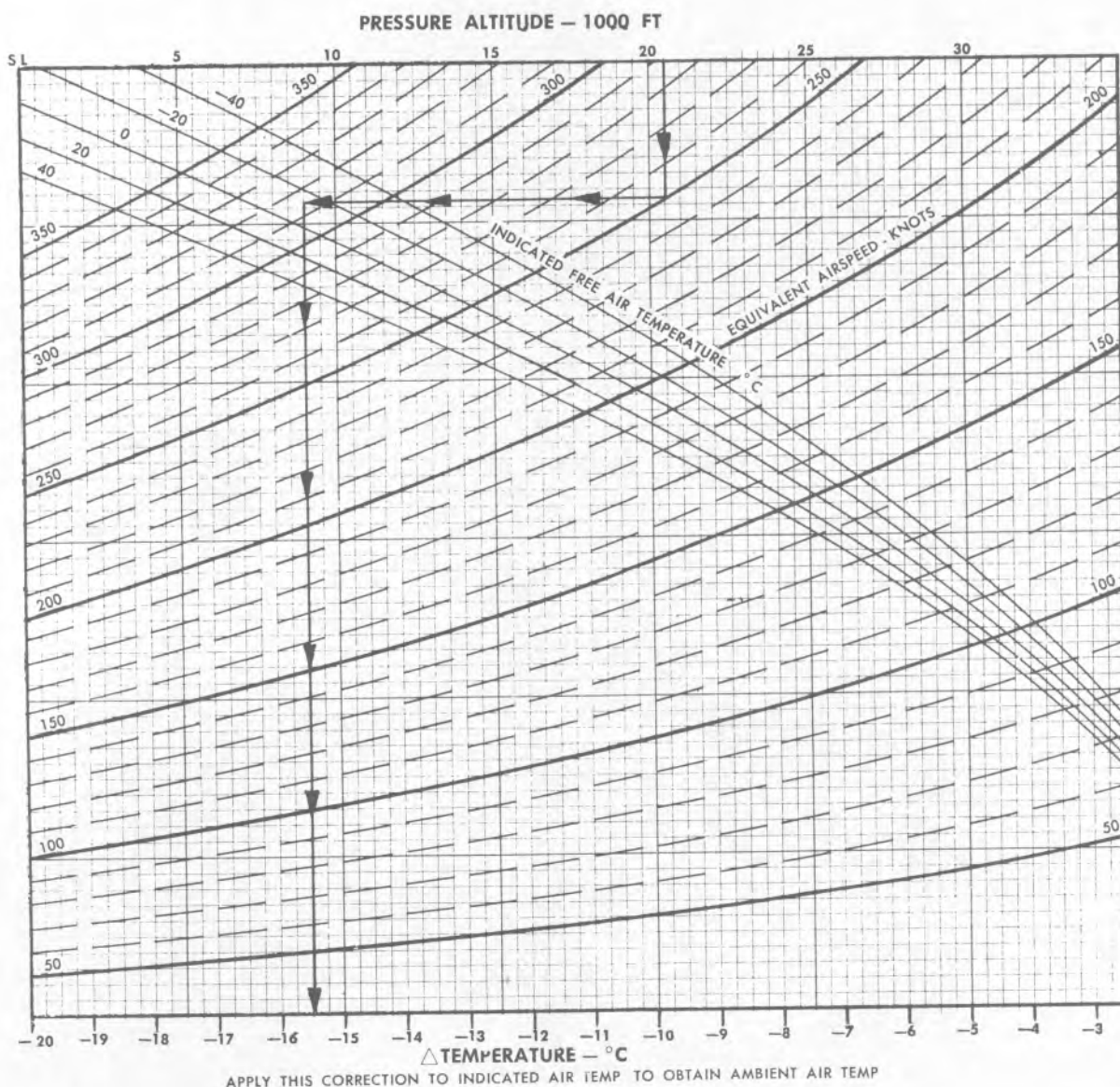


Figure A1-8

TEMPERATURE CONVERSION CHART

$$^{\circ}\text{C} = \frac{5}{9} (^{\circ}\text{F} - 32)$$

$$^{\circ}\text{F} = \frac{9}{5} ^{\circ}\text{C} + 32 = 1.8 (^{\circ}\text{C} + 17.8)$$

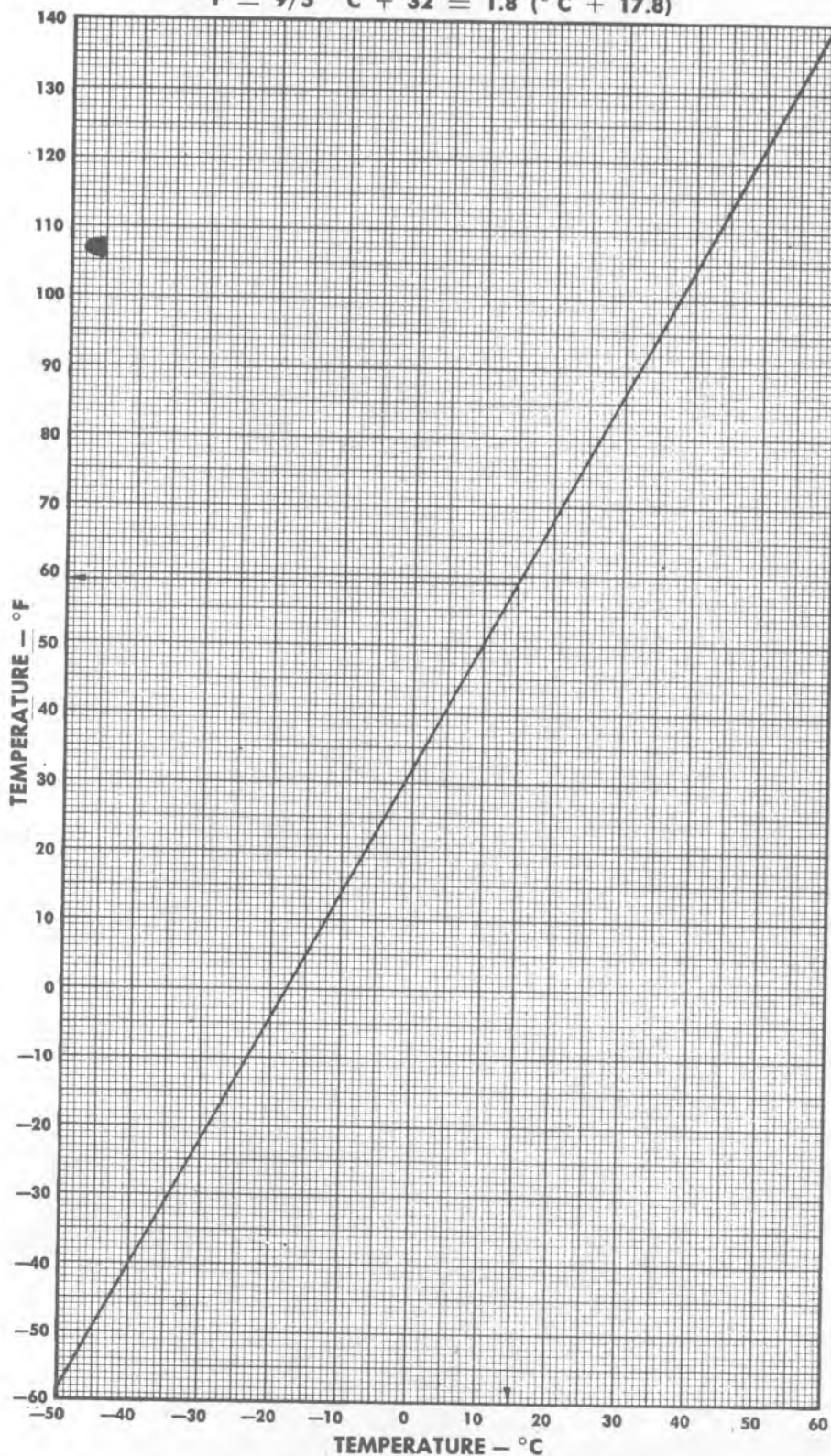


Figure A1-9

STANDARD ATMOSPHERE TABLE

STANDARD S L CONDITIONS:
 TEMPERATURE 15°C(59°F)
 PRESSURE 29.921 IN. HG 2116.216 LB/SQ FT
 DENSITY .0023769 SLUGS/CU FT
 SPEED OF SOUND 1116.39 FT/SEC 661.7 KNOTS

CONVERSION FACTORS:
 1 IN. HG 70.727 LB/SQ FT
 1 IN. HG 0.49116 LB/SQ IN.
 1 KNOT 1.151 M P H
 1 KNOT 1.688 FT/SEC

| ALTITUDE FEET | DENSITY RATIO σ | $\frac{1}{\sqrt{\sigma}}$ | TEMPERATURE | | SPEED OF SOUND KNOTS | PRESSURE | |
|------------------|------------------------------|---------------------------|-------------|---------|----------------------------|--------------|-------------------|
| | | | DEG. C | DEG. F | | IN. OF HG | RATIO δ |
| -4000 | 1.1224 | 0.94390 | 22.925 | 73.265 | 670.7 | 34.5072 | 1.15327 |
| -3000 | 1.0908 | 0.95748 | 20.943 | 69.698 | 668.5 | 33.3107 | 1.11328 |
| -2000 | 1.0598 | 0.97136 | 18.962 | 66.132 | 666.2 | 32.1481 | 1.07442 |
| -1000 | 1.0296 | 0.98552 | 16.981 | 62.566 | 664.0 | 31.0185 | 1.03667 |
| 0 | 1.0000 | 1.00000 | 15.000 | 59.000 | 661.7 | 29.9213 | 1.00000 |
| 1000 | 0.97106 | 1.0148 | 13.019 | 55.434 | 659.4 | 28.8557 | 0.96439 |
| 2000 | 0.94277 | 1.0299 | 11.038 | 51.868 | 657.1 | 27.8210 | 0.92981 |
| 3000 | 0.91512 | 1.0454 | 9.056 | 48.302 | 654.8 | 26.8167 | 0.89624 |
| 4000 | 0.88808 | 1.0611 | 7.075 | 44.735 | 652.5 | 25.8418 | 0.86366 |
| 5000 | 0.86167 | 1.0773 | 5.094 | 41.169 | 650.2 | 24.8959 | 0.83205 |
| 6000 | 0.83586 | 1.0938 | 3.113 | 37.603 | 647.9 | 23.9782 | 0.80138 |
| 7000 | 0.81064 | 1.1107 | 1.132 | 34.037 | 645.6 | 23.0881 | 0.77163 |
| 8000 | 0.78601 | 1.1279 | -0.850 | 30.471 | 643.2 | 22.2249 | 0.74278 |
| 9000 | 0.76196 | 1.1456 | -2.831 | 26.905 | 640.9 | 21.3881 | 0.71481 |
| 10000 | 0.73848 | 1.1637 | -4.812 | 23.338 | 638.5 | 20.5769 | 0.68770 |
| 11000 | 0.71555 | 1.1822 | -6.793 | 19.772 | 636.2 | 19.7909 | 0.66143 |
| 12000 | 0.69317 | 1.2011 | -8.774 | 16.206 | 633.8 | 19.0293 | 0.63598 |
| 13000 | 0.67133 | 1.2205 | -10.756 | 12.640 | 631.4 | 18.2917 | 0.61133 |
| 14000 | 0.65002 | 1.2403 | -12.737 | 9.074 | 629.0 | 17.5773 | 0.58745 |
| 15000 | 0.62923 | 1.2606 | -14.718 | 5.508 | 626.7 | 16.8858 | 0.56434 |
| 16000 | 0.60896 | 1.2815 | -16.699 | 1.941 | 624.2 | 16.2164 | 0.54197 |
| 17000 | 0.58919 | 1.3028 | -18.680 | -1.625 | 621.8 | 15.5687 | 0.52032 |
| 18000 | 0.56991 | 1.3246 | -20.662 | -5.191 | 619.4 | 14.9421 | 0.49938 |
| 19000 | 0.55112 | 1.3470 | -22.643 | -8.757 | 617.0 | 14.3360 | 0.47913 |
| 20000 | 0.53281 | 1.3700 | -24.624 | -12.323 | 614.5 | 13.7501 | 0.45954 |
| 21000 | 0.51496 | 1.3935 | -26.605 | -15.889 | 612.1 | 13.1836 | 0.44061 |
| 22000 | 0.49758 | 1.4176 | -28.586 | -19.456 | 609.6 | 12.6363 | 0.42232 |
| 23000 | 0.48065 | 1.4424 | -30.568 | -23.022 | 607.1 | 12.1074 | 0.40464 |
| 24000 | 0.46416 | 1.4678 | -32.549 | -26.588 | 604.6 | 11.5967 | 0.38757 |
| 25000 | 0.44811 | 1.4938 | -34.530 | -30.154 | 602.2 | 11.1035 | 0.37109 |
| 26000 | 0.43249 | 1.5206 | -36.511 | -33.720 | 599.6 | 10.6274 | 0.35518 |
| 27000 | 0.41729 | 1.5480 | -38.493 | -37.286 | 597.1 | 10.1681 | 0.33983 |
| 28000 | 0.40250 | 1.5762 | -40.474 | -40.852 | 594.6 | 9.7249 | 0.32502 |
| 29000 | 0.38812 | 1.6052 | -42.455 | -44.419 | 592.1 | 9.2975 | 0.31073 |
| 30000 | 0.37413 | 1.6349 | -44.436 | -47.985 | 589.5 | 8.8854 | 0.29696 |

Figure A1-10

DENSITY ALTITUDE AND $1/\sqrt{\sigma}$

| ALTITUDE FEET | $1/\sqrt{\sigma}$ | ALTITUDE FEET | $1/\sqrt{\sigma}$ | ALTITUDE FEET | $1/\sqrt{\sigma}$ | ALTITUDE FEET | $1/\sqrt{\sigma}$ | ALTITUDE FEET | $1/\sqrt{\sigma}$ |
|------------------|-------------------|------------------|-------------------|------------------|-------------------|------------------|-------------------|------------------|-------------------|
| 0 | 1.000 | 6000 | 1.0938 | 12000 | 1.2011 | 18000 | 1.3246 | 24000 | 1.4678 |
| 100 | 1.0015 | 6100 | 1.0955 | 12100 | 1.2030 | 18100 | 1.3269 | 24100 | 1.4704 |
| 200 | 1.0029 | 6200 | 1.0971 | 12200 | 1.2049 | 18200 | 1.3291 | 24200 | 1.4729 |
| 300 | 1.0044 | 6300 | 1.0988 | 12300 | 1.2069 | 18300 | 1.3313 | 24300 | 1.4755 |
| 400 | 1.0059 | 6400 | 1.1005 | 12400 | 1.2088 | 18400 | 1.3335 | 24400 | 1.4781 |
| 500 | 1.0074 | 6500 | 1.1022 | 12500 | 1.2107 | 18500 | 1.3358 | 24500 | 1.4807 |
| 600 | 1.0088 | 6600 | 1.1039 | 12600 | 1.2127 | 18600 | 1.3380 | 24600 | 1.4833 |
| 700 | 1.0103 | 6700 | 1.1056 | 12700 | 1.2146 | 18700 | 1.3403 | 24700 | 1.4860 |
| 800 | 1.0118 | 6800 | 1.1073 | 12800 | 1.2166 | 18800 | 1.3425 | 24800 | 1.4886 |
| 900 | 1.0133 | 6900 | 1.1090 | 12900 | 1.2185 | 18900 | 1.3448 | 24900 | 1.4912 |
| 1000 | 1.0148 | 7000 | 1.1107 | 13000 | 1.2205 | 19000 | 1.3470 | 25000 | 1.4938 |
| 1100 | 1.0163 | 7100 | 1.1124 | 13100 | 1.2224 | 19100 | 1.3493 | 25100 | 1.4965 |
| 1200 | 1.0178 | 7200 | 1.1141 | 13200 | 1.2244 | 19200 | 1.3516 | 25200 | 1.4991 |
| 1300 | 1.0193 | 7300 | 1.1158 | 13300 | 1.2264 | 19300 | 1.3539 | 25300 | 1.5018 |
| 1400 | 1.0208 | 7400 | 1.1175 | 13400 | 1.2284 | 19400 | 1.3561 | 25400 | 1.5045 |
| 1500 | 1.0223 | 7500 | 1.1193 | 13500 | 1.2303 | 19500 | 1.3584 | 25500 | 1.5071 |
| 1600 | 1.0238 | 7600 | 1.1210 | 13600 | 1.2323 | 19600 | 1.3607 | 25600 | 1.5098 |
| 1700 | 1.0253 | 7700 | 1.1227 | 13700 | 1.2343 | 19700 | 1.3630 | 25700 | 1.5125 |
| 1800 | 1.0269 | 7800 | 1.1245 | 13800 | 1.2363 | 19800 | 1.3653 | 25800 | 1.5152 |
| 1900 | 1.0284 | 7900 | 1.1262 | 13900 | 1.2383 | 19900 | 1.3677 | 25900 | 1.5174 |
| 2000 | 1.0299 | 8000 | 1.1279 | 14000 | 1.2403 | 20000 | 1.3700 | 26000 | 1.5206 |
| 2100 | 1.0314 | 8100 | 1.1297 | 14100 | 1.2423 | 20100 | 1.3723 | 26100 | 1.5233 |
| 2200 | 1.0330 | 8200 | 1.1314 | 14200 | 1.2444 | 20200 | 1.3746 | 26200 | 1.5260 |
| 2300 | 1.0345 | 8300 | 1.1332 | 14300 | 1.2464 | 20300 | 1.3770 | 26300 | 1.5287 |
| 2400 | 1.0360 | 8400 | 1.1350 | 14400 | 1.2484 | 20400 | 1.3793 | 26400 | 1.5315 |
| 2500 | 1.0376 | 8500 | 1.1367 | 14500 | 1.2504 | 20500 | 1.3817 | 26500 | 1.5342 |
| 2600 | 1.0391 | 8600 | 1.1385 | 14600 | 1.2526 | 20600 | 1.3840 | 26600 | 1.5370 |
| 2700 | 1.0407 | 8700 | 1.1403 | 14700 | 1.2545 | 20700 | 1.3864 | 26700 | 1.5397 |
| 2800 | 1.0422 | 8800 | 1.1420 | 14800 | 1.2565 | 20800 | 1.3888 | 26800 | 1.5425 |
| 2900 | 1.0438 | 8900 | 1.1438 | 14900 | 1.2586 | 20900 | 1.3911 | 26900 | 1.5453 |
| 3000 | 1.0454 | 9000 | 1.1456 | 15000 | 1.2606 | 21000 | 1.3935 | 27000 | 1.5480 |
| 3100 | 1.0469 | 9100 | 1.1474 | 15100 | 1.2627 | 21100 | 1.3959 | 27100 | 1.5508 |
| 3200 | 1.0485 | 9200 | 1.1492 | 15200 | 1.2648 | 21200 | 1.3983 | 27200 | 1.5536 |
| 3300 | 1.0501 | 9300 | 1.1510 | 15300 | 1.2668 | 21300 | 1.4007 | 27300 | 1.5564 |
| 3400 | 1.0516 | 9400 | 1.1528 | 15400 | 1.2689 | 21400 | 1.4031 | 27400 | 1.5592 |
| 3500 | 1.0532 | 9500 | 1.1546 | 15500 | 1.2710 | 21500 | 1.4055 | 27500 | 1.5620 |
| 3600 | 1.0548 | 9600 | 1.1564 | 15600 | 1.2731 | 21600 | 1.4079 | 27600 | 1.5649 |
| 3700 | 1.0564 | 9700 | 1.1582 | 15700 | 1.2752 | 21700 | 1.4103 | 27700 | 1.5677 |
| 3800 | 1.0580 | 9800 | 1.1600 | 15800 | 1.2773 | 21800 | 1.4128 | 27800 | 1.5705 |
| 3900 | 1.0595 | 9900 | 1.1618 | 15900 | 1.2794 | 21900 | 1.4152 | 27900 | 1.5734 |
| 4000 | 1.0611 | 10000 | 1.1637 | 16000 | 1.2815 | 22000 | 1.4176 | 28000 | 1.5762 |
| 4100 | 1.0627 | 10100 | 1.1655 | 16100 | 1.2836 | 22100 | 1.4201 | 28100 | 1.5791 |
| 4200 | 1.0643 | 10200 | 1.1673 | 16200 | 1.2857 | 22200 | 1.4225 | 28200 | 1.5819 |
| 4300 | 1.0659 | 10300 | 1.1692 | 16300 | 1.2878 | 22300 | 1.4250 | 28300 | 1.5848 |
| 4400 | 1.0676 | 10400 | 1.1710 | 16400 | 1.2899 | 22400 | 1.4275 | 28400 | 1.5877 |
| 4500 | 1.0692 | 10500 | 1.1729 | 16500 | 1.2921 | 22500 | 1.4299 | 28500 | 1.5906 |
| 4600 | 1.0708 | 10600 | 1.1747 | 16600 | 1.2942 | 22600 | 1.4324 | 28600 | 1.5935 |
| 4700 | 1.0724 | 10700 | 1.1766 | 16700 | 1.2963 | 22700 | 1.4349 | 28700 | 1.5964 |
| 4800 | 1.0740 | 10800 | 1.1784 | 16800 | 1.2985 | 22800 | 1.4374 | 28800 | 1.5993 |
| 4900 | 1.0757 | 10900 | 1.1803 | 16900 | 1.3006 | 22900 | 1.4399 | 28900 | 1.6022 |
| 5000 | 1.0773 | 11000 | 1.1822 | 17000 | 1.3028 | 23000 | 1.4424 | 29000 | 1.6052 |
| 5100 | 1.0789 | 11100 | 1.1840 | 17100 | 1.3049 | 23100 | 1.4449 | 29100 | 1.6081 |
| 5200 | 1.0806 | 11200 | 1.1859 | 17200 | 1.3071 | 23200 | 1.4474 | 29200 | 1.6110 |
| 5300 | 1.0822 | 11300 | 1.1878 | 17300 | 1.3093 | 23300 | 1.4499 | 29300 | 1.6140 |
| 5400 | 1.0838 | 11400 | 1.1897 | 17400 | 1.3115 | 23400 | 1.4525 | 29400 | 1.6170 |
| 5500 | 1.0855 | 11500 | 1.1916 | 17500 | 1.3136 | 23500 | 1.4550 | 29500 | 1.6199 |
| 5600 | 1.0871 | 11600 | 1.1935 | 17600 | 1.3158 | 23600 | 1.4576 | 29600 | 1.6229 |
| 5700 | 1.0888 | 11700 | 1.1954 | 17700 | 1.3180 | 23700 | 1.4601 | 29700 | 1.6259 |
| 5800 | 1.0905 | 11800 | 1.1973 | 17800 | 1.3203 | 23800 | 1.4627 | 29800 | 1.6289 |
| 5900 | 1.0921 | 11900 | 1.1992 | 17900 | 1.3224 | 23900 | 1.4652 | 29900 | 1.6319 |

Figure A1-11

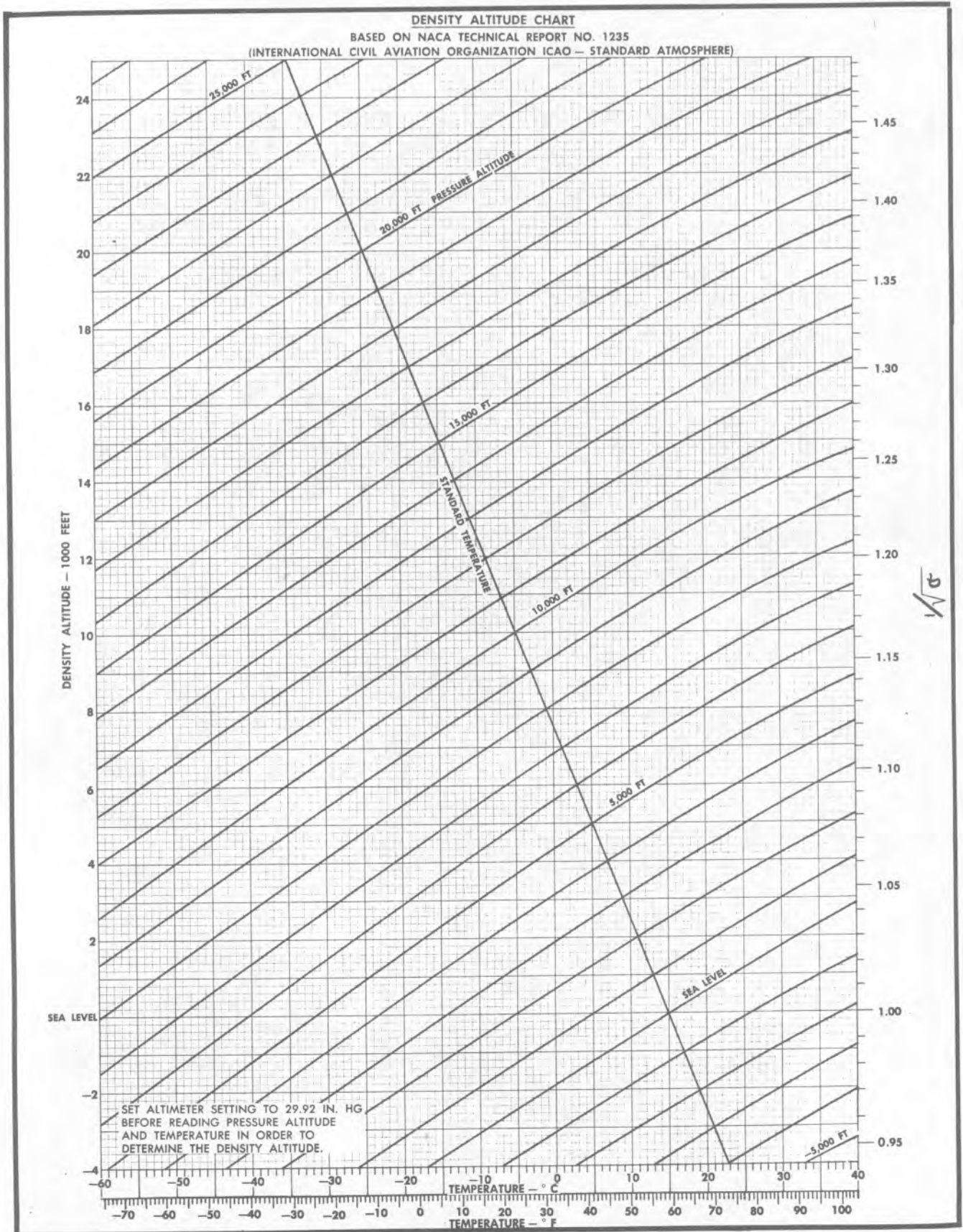


Figure A1-12

PSYCHROMETRIC CHART

VAPOR PRESSURE AND SPECIFIC HUMIDITY DETERMINATION

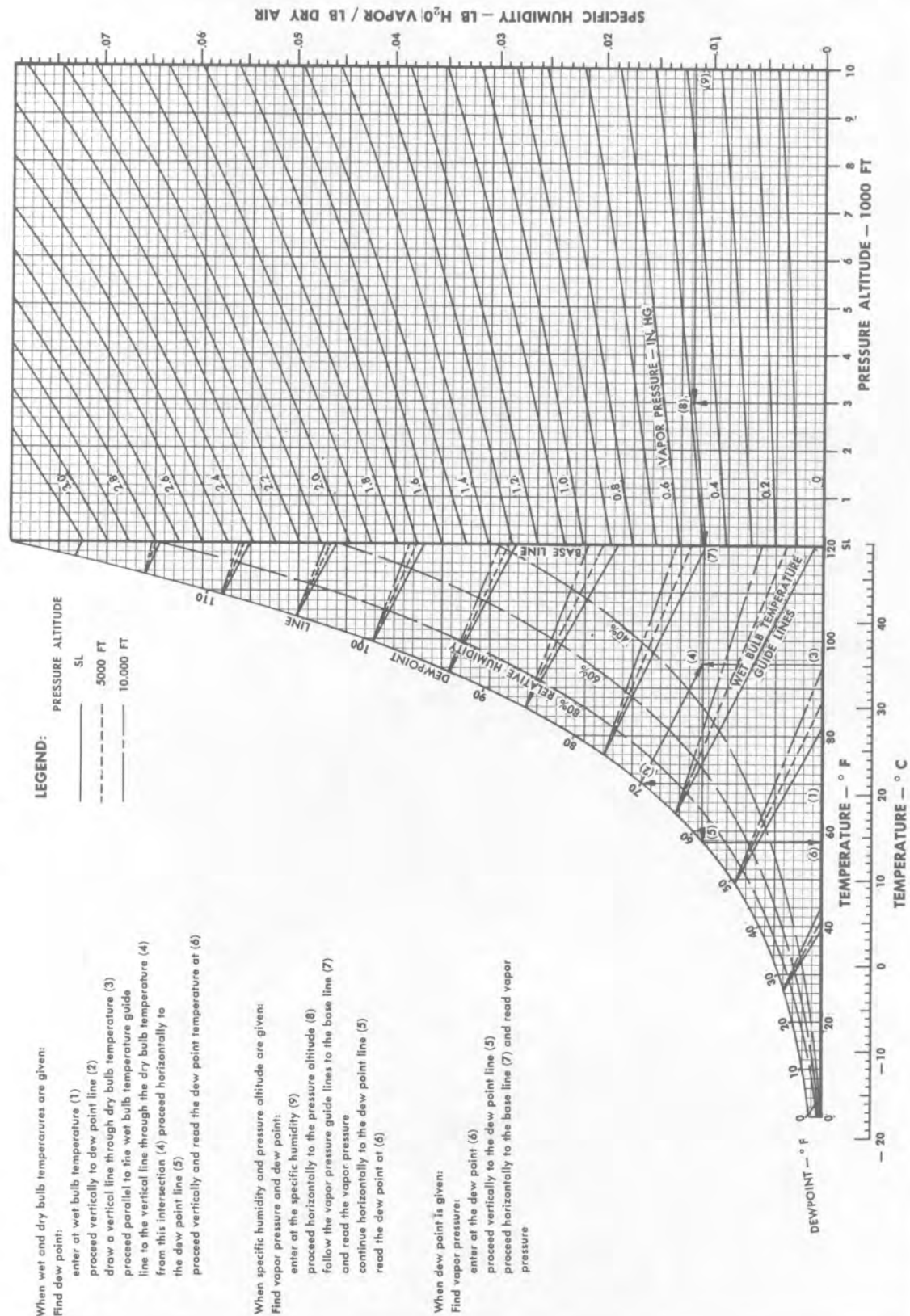


Figure A1-13